MEMORANDUM RM-3054-PR

17 CO

# SIMILARITY SOLUTION FOR CYLINDRICAL MAGNETOHYDRODYNAMIC BLAST WAVES

Carl Greifinger and Julian D. Cole

Reproduced From Best Available Copy

PREPARED FOR:

UNITED STATES AIR FORCE PROJECT RAND

78 47

19991004 119 The RAMD Corporation

SANTA MONICA + CALIFORNIA +---

Han and an odd

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

MEMORANDUM RM-3054-PR JULY 1962

## SIMILARITY SOLUTION FOR CYLINDRICAL MAGNETOHYDRODYNAMIC BLAST WAVES

Carl Greifinger and Julian D. Cole

This research is sponsored by the United States Air Force (wder Project RAND — Contract No. AF 49 (638) 700 — monitored by the Directorate of Development Planning, Deputy Chief of Staff, Research and Technology, Hq USAF. Views or conclusions contained in this Memorandum should not be interpreted as representing the official opinion or policy of the United States Air Force. Permission to quote from or reproduce portions of this Memorandum must be obtained from The RAND Corporation.



#### PREFACE

This work is primarily concerned with the interaction between the flow of an ionized gas and a magnetic field. The particular problem treated corresponds very closely to conditions existing in exploding wire experiments, and should prove useful in interpreting the results of such experiments.

#### SUMMARY

A similarity solution is obtained for the flow behind a very strong (in the hydrodynamic sense) cylindrical magnetohydrodynamic shock wave produced by the sudden release of energy along a line of infinite extent in a plasma. The plasma is assumed to be an ideal gas with infinite electrical conductivity, and to be permeated by the azimuthal magnetic field of a line current. It is shown that it is of critical importance to take into account the ambient magnetic pressure, no matter how small. It is found that, to preserve similarity, the external circuit is required to maintain a constant axial current; this result also appears in the related problem, treated by Greenspan, where the ambient plasma is nonconducting. It is shown that this boundary condition on the circuit implies an exchange of energy at t = 0 between the external circuit and the plasma. When this energy is taken into account, the dependence of the shock speed on the explosive energy can be obtained. This dependence is determined as a function of the ambient magnetic field both for the present case and for Greenspan's case, and interesting differences are noted. The fraction of explosive energy which appears as mechanical energy is also calculated for the two cases, and again significant differences are found to exist. Other differences, with possible experimental consequences, are also discussed. The distributions of flow quantities in the neighborhood of the axis in the present case is found to be different from both the ordinary blast wave and Greenspan's case; the most pronounced differences are in the density distribution for large magnetic field and in the pressure distribution for any magnetic field whatever.

### CONTENTS

PREFACE		111	
SUMMARY		V	
Section I.	INTRODUCTION	1	
II.	FORMULATION OF THE PROBLEM	4	
III.	GENERAL REMARKS	12	
IV.	ORDINARY BLAST WAVE SOLUTION	13	
٧.	PURE MHD CASE	15	
VI.	MODIFIED HYDRODYNAMIC CASE	20	
VII.	ENERGY CONTENT	24	
VIII.	RESULTS AND CONCLUSIONS	27	
REFERENCES			

#### I. INTRODUCTION

It is well known that a similarity solution exists for the flow behind a very strong cylindrical shock wave produced by the sudden release of a finite amount of energy per unit length, along a straight line of infinite extent in a uniform gas. (1) A corresponding magnetohydrodynamic problem also has the same similarity. (2,3,4) Here the shocked gas is an electrically conducting plasma which interacts with an applied magnetic field. The gas is assumed to be initially in a purely azimuthal magnetic field produced by a constant line current, the return for which is a concentric cylindrical conductor of very large radius. The flow is again produced by the sudden release of energy along the axis (by exploding the wire carrying the current, for example).

The flows considered here are those for which the conductivity of the shocked plasma is infinite. For this class of flows, as Greenspan (4) has pointed out, two limiting cases arise. In the first case, the quiescent gas has zero conductivity but the gas behind the shock has infinite conductivity. The magnetic field across the shock is continuous and the boundary conditions at the shock are the ordinary hydrodynamic jump conditions for a strong shock. This situation arises if the magnetic shock transition zone is much wider than the viscous transition zone, which is replaced by a shock jump. The entire effect of the magnetic field, in this case, is contained in its interaction with the flow behind the shock. This limiting case, hereinafter referred to as "modified hydrodynamic," has been discussed by Greenspan. In the second limiting case, the magnetic field is discontinuous across the shock, and the boundary conditions at the shock are those appropriate to a magnetohydrodynamic shock. This

very thin and if the quiescent gas is also a perfect conductor (as a result of pre-ionization, for example). In this case, hereinafter referred to as "pure MHD," the magnetic field affects conditions at the shock itself as well as those behind it.

In this paper, the pure MHD flow is considered in detail. This case was first discussed by Pai, (3) but the results obtained below are found to disagree significantly with his. The discrepancy is shown to arise from an approximation made by Pai to the pressure jump condition at the shock. The particular approximation was to neglect the magnetic pressure in front of the shock. While it is true that, for small values of this magnetic pressure, the errors introduced at the shock are small, nevertheless the inclusion of such a pressure, no matter how small, produces a profound effect at the axis and, concomitantly, in the energy content of the gas.

The question of the energy content of the gas is also considered below, for the modified hydrodynamic as well as for the pure MHD case. It is shown that in both cases, in contrast to the ordinary blast wave solution, the increment in the total (gas dynamic plus magnetic) energy of the gas is not equal to the energy supplied by the explosion. The two cases differ markedly, however, in that in the pure MHD case the increment is infinite, whereas in the modified hydrodynamic case it is finite but leas than the energy supplied by the explosion. The difference between the increment and the explosion energy represents a concentration of magnetic energy, in one case supplied by, and in the other case removed by the external circuit in maintaining the constant current required by the similarity solution—IT is possible in both cases to calculate the contribution from

the external circuit, and thereby to relate the shock speed and the mechanical energy in the gas to the energy supplied by the explosion. The analysis reveals an interesting difference between the two cases. In both cases only part of the energy supplied by the explosion appears as mechanical energy, the remainder being converted to magnetic energy. In the pure MHD case, this converted part of the explosion energy appears in the compressed magnetic field behind the shock, while in the modified hydrodynamic case, it is delivered instead to the external circuit.

It seems reasonable to believe that, despite the divergence mentioned above, the results obtained have physical significance. The divergence appears because of the unphysical assumption of a dimensionless axial conductor. One would expect that in any actual experiment, where the axial conductor has a finite radius, the true flow would approach that given by the similarity solution at distances from the axis much greater than the radius of the conductor. One would also expect that any relations obtained between finite quantities, such as the dependence of the shock speed on the explosion energy or the ratio of mechanical energy to explosion energy, would also be approximately valid. There are questions which, of course, must ultimately be decided experimentally.

#### II. FORMULATION OF THE PROBLEM

A solution of the magnetohydrodynamic equations is desired for the flow behind a cylindrical shock wave produced by the sudden release of a finite amount of energy E<sub>O</sub> per unit length, along an axis of infinite extent in a plasma. The plasma is assumed to be an ideal gas with infinite electrical conductivity; viscosity and heat conduction are neglected. An azimuthal magnetic field is assumed to exist initially in the plasma. As a consequence of the assumption of infinite conductivity, the magnetic field in the plasma remains azimuthal. Under the assumptions made, all quantities are functions only of the radius r and time t, and the motion of the gas is governed by the following equations:

$$r \frac{\partial \rho}{\partial t} + \frac{\partial}{\partial r} (r\rho u) = 0$$
 (continuity) (la)

$$\frac{\partial u}{\partial t} + u \frac{\partial u}{\partial r} + \frac{1}{\rho} \frac{\partial p}{\partial r} + \frac{1}{\rho} \frac{\partial}{\partial r} \left( \frac{B_Q^2}{2\mu} \right) + \frac{B_Q^2}{\rho \mu r} = 0 \qquad \text{(momentum)}$$

$$\frac{\partial B_0}{\partial t} + \frac{\partial}{\partial r} (uB_0) = 0$$
 (induction) (le)

$$\left(\frac{\partial}{\partial t} + u \frac{\partial}{\partial r}\right) \left(\frac{p}{\rho^{\gamma}}\right) = 0$$
 (entropy). (1d)

In these equations, p is the gas pressure,  $\rho$  is the density, u the radial velocity, and  $B_Q$  the azimuthal magnetic field. The specific heat ratio  $\gamma$  is assumed constant and the magnetic permeability  $\mu$  is taken to be that of free space (MKS units are used throughout). The gas is assumed to be initially in a uniform state  $p_Q$ ,  $\rho_Q$ . The initial azimuthal magnetic field is assumed to be that produced by a constant current  $I_Q$ , flowing along the axis.

Entering into the initial and boundary conditions of the problem are certain dimensional constants; these are the initial pressure  $p_0$ , the initial density  $\rho_0$ , the initial axial current  $I_0$ , and the energy  $E_0$  liberated per unit length. Since the dimensions of the quantity  $\mu I_0^2$  are the same as those of  $E_0$ , only three of the four constants are dimensionally independent. If, in addition, the liberated energy  $E_0$  is large enough to produce a very strong shock, the initial pressure  $p_0$  may be neglected, and only two constants with independent dimensions enter into the problem-- $\rho_0$  and  $E_0$ . As in the ordinary blast wave case, the only combination of length and time that can be formed from these constants is of the form

$$\frac{(length)^2}{time} \sim \sqrt{\frac{E_o}{\rho_o}}$$
.

It now follows from general considerations that the system of equations, (1), possesses a similarity solution; this solution is of the form

$$\rho = \rho_0 \mathcal{L}(\eta) \tag{2a}$$

$$u = \frac{r}{t} \mathcal{U}(\eta) \tag{2b}$$

$$p = \rho_0 \left(\frac{r}{t}\right)^2 \mathscr{P}(\eta) \tag{2c}$$

$$B_0 = (\mu \rho_0)^{\frac{1}{2}} \frac{r}{t} \mathcal{B}(\eta) \tag{2d}$$

where  $\ell$ , u,  $\ell$  and  $\ell$  are non-dimensional functions of a non-dimensional variable. The only non-dimensional variable which can be formed from the variables r and t and the dimensional constants of the problem is the variable

$$\eta = \frac{r^2}{c^*t} \tag{3}$$

where c\* is some characteristic parameter with the dimensions of (length)<sup>2</sup>/time.\*

It is convenient to introduce as independent variables, instead of r and t, the stream function # defined by

$$\frac{\partial \psi}{\partial r} = \frac{\rho}{\rho_0} r , \quad \frac{\partial \psi}{\partial t} = -\frac{\rho}{\rho_0} ur$$
 (4)

and the variable of defined as

$$\phi = \frac{2\psi}{r^2} . \tag{5}$$

Physically, the value of  $\not 0$  corresponding to any (r,t) is the ratio of the mass between the axis and the radius r at time t to the mass initially in the same volume. The value of  $\not 0$  at the shock, therefore, is  $\not 0_8 = 1$ . A line of constant  $\not 0$  is also a line of constant  $\eta$  in the (r,t) plane.

In terms of the variables  $(\psi, \emptyset)$ , Eqs. (2) take the form

$$\rho = \rho_0 \, \sigma(\phi) \tag{6a}$$

$$u = e^{-\frac{U(p)}{\sqrt{1/2}}}$$
 (6b)

$$p = \rho_0 e^{-2} \frac{P(p)}{\phi}$$
 (6e)

$$B_0 = (\mu \rho_0)^{1/2} \frac{c^*}{\sqrt{1/2}} \beta(\phi)$$
 (6d)

The quantity  $\eta$  defined by Eq. (3) is proportional to the square of that defined by Greenspan.

where the quantities  $\sigma$ , U, P, and  $\beta$  are non-dimensional functions of the single (non-dimensional) variable  $\phi$ . The parameter  $c^*$  in Eq. (6) is related to the speed of the shock; in general,

$$c = A \frac{c^*}{\sqrt{1/2}}$$
 (7)

where c is the shock speed and A is an arbitrary constant. In the present case, it is convenient to choose A = 1.

It is necessary for the initial conditions to be compatible with the assumed form, (6), of the solution. The plasma is assumed to be initially at rest, to have a uniform density  $\rho_0$ , a uniform pressure  $\rho_0$ , and to be permeated by the azimuthal magnetic field of a constant line current  $I_0$ . The first two conditions are obviously expressible in the desired form; viz.,

$$U_0 = 0$$
 (8a)

and

respectively, while the last condition can be written in the form

$$\beta_{o} = \left(\frac{\mu I_{o}^{2}}{8\pi^{2}\rho_{o}e^{+2}}\right)^{1/2} . \tag{8e}$$

For the condition of uniform pressure to be compatible with (6), however, it is necessary to assume that the initial pressure is negligible; i.e.

$$p_0 = 0$$
. (8d)

This is the usual blast wave assumption of a very strong shock.

The Jacobian of the transformation defined by Eqs. (4) and (5) is

$$J = \frac{\partial(\phi, \phi)}{\partial(r, t)} = -2 \operatorname{\sigma u}\phi . \tag{9}$$

Since the Jacobian is not zero (except at certain points), the transformation defines a one-to-one mapping between (r,t) and  $(\psi,\phi)$ . One may, in fact, obtain an integral expression for the stream function  $\psi$ . The differential equation

$$\frac{\partial t}{\partial \phi} = -\frac{1}{J} \frac{\partial \phi}{\partial r} = \frac{1}{2^{1/2} c^*} \frac{\sigma - \phi}{\sigma \phi^{1/2} U}$$
 (10)

is easily integrated to yield

$$\psi = 2^{1/2} c^* t \frac{\sigma p^{1/2} U}{\sigma - p}$$
 (10a)

Finally, it is possible to express the variable  $\eta$  as a function (implicit) of  $\beta$ ; by combining Eqs. (3), (5) and (10), one obtains

$$\eta = 2^{3/2} \frac{\sigma U}{\phi^{1/2} (\sigma - \phi)} \tag{11}$$

If one now substitutes Eq. (6) into Eqs. (1) and transforms the partial derivatives to derivatives with respect to  $\emptyset$ , the equations of motion become

$$2\phi^{3/2}U\frac{d}{d\phi}\left(\frac{\sigma}{\phi^{1/2}}\right) + \frac{\sigma^2U}{\phi} + 2(\phi-\sigma)\sigma\frac{dU}{d\phi} = 0 \qquad (continuity) \qquad (12a)$$

$$\dot{p}^2 U \frac{dU}{d\dot{p}} + \frac{\dot{p}}{\sigma} (\dot{p} - \sigma) \frac{d}{d\dot{p}} (P + \frac{1}{2} \beta^2) + (P + \frac{1}{2} \beta^2) - \frac{\dot{p}\beta^2}{2\sigma} = 0 \quad (momentum) \quad (12b)$$

$$2\phi U \frac{d\beta}{d\phi} + \frac{\beta \sigma U}{\phi} + 2(\phi - \sigma) \beta \frac{dU}{d\phi} = 0$$
 (induction) (12c)

$$\frac{\mathrm{d}}{\mathrm{d}\emptyset} \left( \frac{\mathrm{P}}{a^7} \right) = 0 \tag{entropy} . \tag{12d}$$

A solution of Eqs. (12) is desired which satisfies the boundary conditions appropriate to a very strong magnetohydrodynamic shock. In terms of physical variables, these conditions may be written:

$$\frac{\rho_0}{\rho_s} = 1 - \frac{u_s}{c} \qquad (continuity) \qquad (13a)$$

$$p_{s} + \frac{1}{2u} (B_{s}^{2} - B_{o}^{2}) = \rho_{o} u_{s} c$$
 (momentum) (15b)

$$\frac{B_0}{B_0} = 1 - \frac{u_s}{c}$$
 (induction) (13c)

$$(c^2 - \frac{\gamma+1}{2} cu_s)(c-u_s)^2 = \frac{B_0^2}{\mu\rho_0} (c^2 - \frac{\gamma+1}{2} cu_s + \frac{\gamma}{2} u_s^2)$$
 (wave speed) (15d)

where the subscript "s" denotes quantities immediately behind the shock and  $B_{C}$  is the value of  $B_{C}$  immediately shead of the shock. The quantity c is again the shock speed, given by (7% with A = 1). The wave speed equation, (13d), is derived by combining the usual energy equation with the continuity, momentum and induction equations.

It should be noted that the magnetic pressure ahead of the shock has been retained in the momentum equation, (1%). Although it is necessary to neglect the ambient gas pressure in this equation to preserve similarity, the same is not true of the ambient magnetic pressure which does have the proper form. This term, which was neglected by Pai, can therefore be retained and, as will be shown below, should be retained.

In terms of the non-dimensional variables defined by Eq. (6), the shock relations become:

$$\frac{1}{\sigma_{\rm g}} = 1 - U_{\rm g} \tag{14a}$$

$$P_{s} + \frac{1}{2} \beta_{0}^{2} (\sigma_{s}^{2} - 1) = U_{s}$$
 (14b)

$$\frac{\beta_0}{\beta_0} = 1 - U_B \tag{14c}$$

$$(1 - \frac{\gamma+1}{2} U_s)(1 - U_s) = \beta_0^2 (1 - \frac{\gamma}{s} U_s). \qquad (14d)$$

The quantity  $\beta_0$  is given by Eq. (8c), and is, physically, the ratio of the Alfvén speed in the gas immediately shead of the shock to the shock speed (Alfvén number).

If  $\beta_0$  is considered a parameter, Eqs. (14) define a one-parameter family of shock curves. For a given value of  $\beta_0$ ,  $U_g$  is first determined as a root of the quadratic equation, (14d). One then obtains  $\sigma_g$  and  $\beta_g$  directly from Eqs. (14a) and (14c), respectively, and then  $P_g$  from Eq. (14b).

Three algebraic integrals of the four equations of motion may be obtained. The entropy equation, (12d), has the immediate integral

$$\frac{P}{\sigma^7} = a = (constant) \tag{15}$$

from which it follows that the entropy is constant along a streamline. A second integral may be obtained by combining Eqs. (12a) and (12c); namely

$$\beta^2 \frac{\emptyset}{\sigma^2} = 2b = (constant) \tag{16}$$

which expresses the fact that the field is "frozen" into the fluid -- a

well-known consequence of the assumption of infinite conductivity. A final algebraic integral, obtained by combining Eqs. (12a) and (12b), is

$$\frac{1}{\sigma} \left( \frac{P}{\gamma - 1} + \frac{1}{2} \beta^2 + \frac{1}{2} \sigma U^2 \right) + \frac{\phi - \sigma}{\sigma \phi} \left( P + \frac{1}{2} \beta^2 \right) = k = \text{(constant)}.$$
 (17)

This so-called "energy integral" results from the fact that, with the assumed similarity, the total energy is constant not only for the entire flow field, but also between any two similarity lines.

To establish the connection between the variables used here and those of Greenspan, one additional relation may be derived; from Eqs. (11) and (14a), the value of  $\eta$  at the shock is  $\eta_s = 2^{5/2}$ . It then follows from Eq. (3) that the location of the shock is at  $r_s(t) = 2^{3/4}(c^*t)^{1/2}$ .

The three integrals (15), (16) and (17) may now be used to eliminate the functions P,  $\beta$  and U from Eqs. (12). The system, (12), is thereby reduced to the single first order equation

$$\frac{d\xi}{d\sigma} = \frac{\xi}{\sigma(1-\xi)} \frac{a\sigma^{\gamma-1}(\xi - \frac{\gamma}{\gamma-1}) \left[ (\gamma-2)\xi - \gamma \right] - (1+\xi) \left[ k + b\xi(\xi-2) \right]}{a\sigma^{\gamma-1}(2\xi - \frac{\gamma}{\gamma-1}) + b\xi(3\xi - 4) + k}$$
(18)

where

$$\xi = \frac{\sigma}{\rho} \ . \tag{19}$$

If neither a nor b is zero, no further analytic integration appears possible. In the general case, then, the problem is reduced to the numerical integration of a single ordinary equation.

#### III. GENERAL REMARKS

A few general remarks can be mede in connection with Eq. (18).

Both cases mentioned in the Introduction, i.e., pure MHD, and modified hydrodynamic, as well as the ordinary blast wave, appear as special cases of Eq. (18). The solution, in each case, is that integral curve of Eq. (18) which starts at the point appropriate to the particular shock and terminates at the point which corresponds to the axis. (Each point on the integral curve maps into a line of constant η in the (r,t)-plane.)

In every case, the point corresponding to the shock is a regular point of the differential equation. Since only a single integral curve may pass through a regular point, the solutions obtained in this manner are unique.

A point of central importance in the analysis is the dependence of the solution on conditions at the shock. The boundary conditions at the shock enter into Eq. (18) through the constants a, b, and k, which are determined by evaluating the integrals (15), (16), and (17) at the shock. Because of the non-linearity of Eq. (18), these constants affect the entire flow behind the shock in a very complicated way. The most striking effect, however, is on conditions at the axis. An axis of symmetry always corresponds to a singular point of such a differential equation, i.e., to a point at which both the numerator and denominator vanish. The behavior of physical quantities at the axis is very sensitive to the location of this singular point, which, in turn, is determined by the relationships among the constants a, b, and k prescribed by conditions at the shock. As will be seen below, this sensitivity to the location of the singular point manifests itself in a profound difference at the axis, especially in the pressure distribution, between the pure MID and modified hydrodynamic cases.

#### IV. ORDINARY BLAST WAVE SOLUTION

For purposes of illustration and comparison, the ordinary blast wave solution in the present variables is briefly sketched below. The blast wave solution is recovered in the limit of zero magnetic field. The appropriate shock conditions are Eqs. (14) with  $\beta_0 = 0$ . These, applied to Eqs. (15) through (17), yield  $\alpha = \frac{2}{\gamma+1} \left(\frac{\gamma-1}{\gamma+1}\right)^{\gamma}$ ,  $\alpha = 0$ ; the integrals (15) and (17) therefore become

$$P = \frac{2}{\gamma+1} \left( \frac{\gamma-1}{\gamma+1} \right)^{\gamma} \sigma^{\gamma}$$
 (20)

and

$$\frac{1}{2} \sigma U^2 + (\frac{\gamma}{\gamma - 1} - \xi) P = 0 , \qquad (21)$$

respectively, with \$ defined by Eq. (19).

The singular point of Eq. (18) corresponding to the axis in this case is the saddle point  $\sigma=0$ ,  $\xi=\frac{\gamma}{\gamma-1}$ . The behavior of physical quantities in the neighborhood of the axis can be deduced from an analysis of Eq. (18) in the neighborhood of the singular point. However, in this case Eq. (18) can be integrated analytically; the solution satisfying the boundary conditions at the shock is

$$\sigma = \left(\frac{\gamma-1}{2}\right)^{\frac{2}{2-\gamma}} \left(\frac{\gamma+1}{\gamma-1}\right)^{\frac{\gamma}{\gamma}} \left[\frac{(\gamma-1)\xi-\gamma}{\xi}\right]^{\frac{1}{\gamma}} \left[(\gamma-\gamma)\xi+\gamma\right]^{\frac{2}{2-\gamma}}.$$
 (22)

Equations (20)-(22) give the complete solution, in parametric form, of the equations of motion. The parameter  $\xi$  decreases monotonically from the value  $\frac{\gamma+1}{\gamma+1}$  at the shock to the value  $\frac{\gamma}{\gamma-1}$  at the axis.

It can be seen from these equations that P and U both become zero  $\frac{(2\gamma-1)}{2}$  at the axis, with  $P \sim \sigma^{\gamma}$  and  $U \sim \sigma^{-2}$ . Since  $\phi = \sigma \ \xi \sim \sigma$  at the axis, it follows from Eq. (10a) that  $\psi \sim \sigma^{\gamma} t$ , and consequently from Eqs. (6) for the physical variables, that  $\rho \to 0$ ,  $u \to 0$ , and  $pt \to constant$  at the axis. These are well-known properties of the blast wave solution.

#### V. PURE MHD CASE

In the pure MHD case, the boundary conditions at the shock are given by Eqs. (14) with  $0 < \beta_0 < 1$ . (The density ratio across the shock decreases with increasing  $\beta_0$ , becoming unity when  $\beta_0 = 1$ .) These shock conditions, applied to Eqs. (16) and (17), yield

$$b = k = \frac{1}{2} \beta_0^2. \tag{23}$$

When these values of b and k are substituted into Eq. (18), it is found that a higher order singular point  $\sigma = 0$ ,  $\xi = 1$  corresponds to the axis. The parameter  $\xi$  decreases monotonically from its value at the shock to its value at the axis.

An interesting conclusion can already be drawn from the location of the singular point. It is easy to show, from the various defining relationships and the integral (16) with  $b=\frac{1}{2}\,\beta_0^2$ , that the magnetic field behind the shock is given by

$$B_{Q}(\mathbf{r},t) = \frac{\mu I_{Q}}{2\pi r} f(\mathbf{r},t) . \qquad (24)$$

The factor multiplying the parameter  $\xi$  in Eq. (24) is clearly the initial magnetic field. Thus, as might be expected, the magnetic field is everywhere compressed between the shock and the axis. At the axis, however, the magnetic field maintains its initial value. This implies that, to preserve similarity, the external circuit must maintain a constant current  $I_0$ . (The same result was obtained by Greenspan in the modified hydrodynamic case.) One might expect a priori that a flow with the same similarity would be produced if the current in the wire were instantaneously increased

to a new constant value I, since such a boundary condition introduces no new dimensional constants and is expressible in a form compatible with the similarity. This, however, is apparently not the case; only the maintenance of a constant current preserves similarity.

Because of the high order singularity of Eq. (18) at  $\sigma = 0$ ,  $\xi = 1$ , the dependence of the other variables on \$ in the neighborhood of the axis is most easily determined from the continuity equation, (12a). An analysis of this equations shows that, in the neighborhood of  $\sigma = 0$ ,  $\xi = 1$ ,

$$U = U_0 \exp \left[ -\left(\frac{2}{\gamma - 1}\right) \left(\frac{1}{\xi - 1}\right) \right]$$
 (25)

where  $U_0$  is a constant. It then follows from equations (17), (10a), and (11) that

$$\sigma = \sigma_1(\xi - 1)^{\frac{2}{\gamma - 1}} \tag{26a}$$

$$\sigma = \sigma_{1}(\xi - 1)^{\frac{2}{\gamma - 1}}$$

$$\uparrow = \uparrow_{0} t (\xi - 1)^{\frac{2}{\gamma - 1}} \exp \left[ -\frac{2}{(\gamma - 1)} \frac{1}{(\xi - 1)} \right]$$
(26a)

$$\eta \approx \eta_0(\xi - 1)^{-\frac{\gamma}{\gamma - 1}} \exp \left[ -\frac{2}{(\gamma - 1)} \frac{1}{(\xi - 1)} \right]$$
 (26c)

where  $\sigma_1 = \left[ (\gamma - 1) \frac{b}{a} \right]^{\frac{1}{(\gamma - 1)}}$ , and  $\phi_0$  and  $\phi_0$  are constants. The last of these equations verifies that this singular point indeed corresponds to the exis (7 = 0).

The behavior of the physical variables in the neighborhood of the axis can now be deduced from the defining equations, (6), and the integrals (15) and (16). The results are:

$$\rho = \rho_0 \sigma_1 \left[ -\ln \eta^2 \right] - \frac{2}{(\gamma - 1)}$$
(27a)

$$u \approx \left(\frac{c^*}{t}\right)^{1/2} \frac{1}{(\gamma-1)} \eta^{\frac{1}{2}} \left[-\ln \eta\right]^{-1}$$
 (27b)

$$p \approx \frac{\rho_0 c^+}{c} \frac{8b}{(7-1)} \eta^{-1} \left[ -\ln \eta \right]^{-2}$$
 (27c)

$$\frac{B^2}{2\mu} = \frac{p_0 c^*}{t} 2b \eta^{-1}. \tag{27d}$$

As in the ordinary blast wave solution, the density and velocity, approach zero at the axis. The dependence on  $\eta$ , however, is quite different in the two cases, the logarithmic dependence being peculiar to the pure MHD case. The density, in particular, approaches zero much more slowly in the pure MHD case, especially for the larger values of  $\beta_0$  (Fig. 1). The pressure is markedly different, becoming infinite at the axis rather than asymptotically constant as in the blast wave solution (Fig. 3). This infinity will be discussed further in connection with the energy content of the gas.

The results of the numerical integration of Eq. (18) for various values of  $\beta_0^2$ , with  $\gamma=1.4$ , are shown in Figs. 1-4. It is clear that the presence of a magnetic field shead of the shock has an important effect on conditions at the shock (and everywhere behind it) as well as those at the axis. The compression across the shock decreases from its strong-shock value of  $\frac{\gamma+1}{\gamma+1}$  for zero magnetic field ( $\beta_0=0$ ) to a value of unity for  $\beta_0=1$ . The velocity and gas pressure at the shock vary accordingly, decreasing from their strong-shock values to zero over the range of  $\beta_0$ . (The similarity

solution is valid, of course, only so long as the shock remains a strong shock in the hydrodynamic sense, that is, so long as the gas pressure ahead of the shock is negligible compared to that behind it.) The magnetic pressure at the shock, on the other hand, exhibits a maximum at a value of  $\beta_0^2$  between 0.3 and 0.4. The appearance of such a maximum was noted in the inverse pinch effect. The existence of this maximum depends only on the jump conditions at the shock, which are the same as in the inverse pinch.

The importance of including the ambient magnetic pressure in the shock relations is illustrated by comparison of the above results with those of Pai, where this term was neglected. In the first place, if the ambient magnetic pressure is neglected in Eq. (14b), the Alfvén number,  $\beta_{c}$ , is allowed to become arbitrarily large. This is in contradiction to the limits  $0 < \beta_0 < 1$  obtained above for a pure MHD shock. In the second place, all hydrodynamic quantities at the shock become independent of  $\beta_{\alpha}$ , always attaining their strong-shock values. It can be seen from Figs. 1-3 that this is a reasonable approximation only for very small values of  $\beta_{\alpha}$ . The same error is introduced into the magnetic field ratio across the shock which, with Pai's conditions, is always  $\frac{\gamma+1}{\gamma-1}$  but which, with Eqs. (14), decreases from this value to unity at  $\beta_0 = 1$ . Finally, and what is responsible for an important discrepancy even for the smallest values of  $\beta_{c}$ , Pai's conditions lead to different values for the constants a, b, and k of Eqs. (15)-(17), and thereby alter the location of the singular point of Eq. (18) which corresponds to the axis. With Pai's conditions, the singular point is located at  $\sigma=0$ ,  $\xi=\frac{\gamma+1}{\gamma-1}$  rather than at  $\sigma=0$ , § = 1 (which is no longer even a singular point of the differential) equation). Along the integral curve passing through the shock, the

variable  $\xi$  decreases from its value of  $\frac{\gamma+1}{\gamma-1}$  at the shock to some minimum value, and then increases back to this value at the axis. Since the magnetic field behind the shock is given by Eq. (24), the location of the singular point implies that the current in the wire has jumped to  $\frac{\gamma+1}{\gamma-1}$  times its initial value, a solution in contradiction to the requirement of a constant current when the ambient magnetic pressure is retained. The difference in location of the singular point also leads to discrepancies in the behavior of the other physical variables near the axis. In Pai's solution, the density and velocity go to zero at the axis, but with a dependence on  $\eta$  which is quite different from that given by Eqs. (27a) and (27b). The most dramatic difference, however, is in the pressure which, rather than becoming infinite, as given by Eq. (27c), goes to zero at the axis! The solution in the neighborhood of the axis thus shows a sensitivity to the shock conditions which is more than a little surprising.

#### VI. MODIFIED HYDRODYNAMIC CASE

The modified hydrodynamic case has been considered in detail by Greenspan, who obtained the solution by the numerical integration of three coupled differential equations combined with one integral of the motion. The solution can also be obtained within the framework of the present formalism. Some properties of the solution of interest for comparison with the pure MHD case and for the energy considerations to follow, are briefly noted at this point. In this case, the magnetic field is assumed to be continuous across the shock; the boundary conditions at the shock are therefore simply the ordinary hydrodynamic strong-shock conditions, and the effect of the magnetic field appears only in the flow behind the shock. The range of the Alfvén number,  $\beta_0$ , is now indeed unbounded, in contrast with the pure MHD case.

When the strong shock conditions, together with the continuity of the magnetic field, are applied to Eqs. (16) and (17), one obtains

$$b = \frac{1}{2} \beta_0^2 \cdot \left(\frac{\gamma - 1}{\gamma + 1}\right)^2$$
 (28a)

$$k = \frac{(\gamma - 3)(\gamma + 1)}{(\gamma - 1)^2} b$$
 (28b)

(cf., Eq. (23) for the pure MHD case). The singular point of Eq. (18) which corresponds to the axis is the point  $\sigma=0$ ,  $\xi=\frac{\gamma+1}{\gamma-1}$ . Along the integral curve through the shock, the parameter  $\xi$  decreases from its value at the shock,  $\xi_{\rm s}=\frac{\gamma+1}{\gamma-1}$ , to some minimum value, and then increases back to

This was only a special case of the more general problem of finite conductivity, treated by Greenspan, where the entropy and frozen field integrals do not exist.

this value at the axis. In the modified hydrodynamic case, the magnetic field behind the shock is given by

$$B_{Q}(r,t) = \frac{\mu I_{Q}}{2\pi r} \frac{\xi(r,t)}{\xi_{g}}$$
 (29)

(cf., Eq. (24)). Thus, the field is everywhere smaller between the shock and the axis than it was initially; the field is expanded by the shock rather than compressed by it as in the pure MHD case. At the axis, the field again maintains its initial value, so that, as in the pure MHD case, a requirement for similarity is that the external circuit maintain a constant current.

This difference in the variation of the magnetic field implies a marked difference between the two cases in the current distributions in the shocked gas. In both cases, the field ahead of the shock is assumed to remain unaltered; the integrated current through the gas must therefore be zero in both cases. In the pure MHD case, where the field jumps across the shock, there is a cylindrical current sheet along the shock front, flowing in the same direction as the axial current, and balanced by opposite currents in the remainder of the gas. In the modified hydrodynamic case, where the field is continuous across the shock, there is no current sheet. Between the shock and the point where the variable \( \xi\$ reaches its minimum value, there are currents in the gas flowing in the same direction as the axial current; these are balanced by the opposite currents in the remainder of the gas.

Although the singular point of Eq. (18) for Pai's solution is the same as that for Greenspan's solution, a current jump is implied in the former case, but a constant current in the latter. The reason for this is that Pai's jump condition for the magnetic field leads to a value of b given by Eq. (25) rather than Eq. (28a), and hence to an expression for  $B_a$  given by Eq. (24) rather than Eq. (29).

Another important difference between the two cases is in the behavior of the other physical variables in the neighborhood of the axis. The density and velocity again become zero at the axis, but not with the logarithmic dependence on  $\eta$  of Eqs. (27a) and (27b). The pressure, however, also goes to zero at the axis, in contrast to the pure MHD case where it becomes infinite. The results for these two cases, as well as for the ordinary blast wave, are summarized in Table 1.

Table 1 DEPENDENCE OF PHYSICAL VARIABLES ON NON-DIMENSIONAL VARIABLE  $\eta$  — IN THE NEIGHBORHOOD OF THE AXIS (  $\eta$   $\rightarrow$  0 )

Case Variable	Pure MHD	Modified Hydrodynamic	Ordinary Blast Wave
ρ	$\begin{bmatrix} \frac{(\gamma-1)}{2} \end{bmatrix}^{-\frac{2}{(\gamma-1)}}$	η <sup>2</sup> 7-1	η <del>1</del> γ-1
ut <sup>1/2</sup>	$\eta^{1/2} \left[ - \ln \eta \right]^{-1}$	η1/2	ŋ1/2
pt	η-1 [- ln η] -2	ŋ	const.

#### VII. ENERGY CONTENT

The one remaining parameter of the problem is the explosive energy per unit length,  $E_0$ , released along the axis at t=0. This parameter enters through the fact that, with the assumed similarity, the total energy between any two similarity lines, in particular between the shock and the axis, is constant in time. In the ordinary blast wave solution, the initial energy of the gas is assumed negligible and the gas is assumed isolated from all external energy sources. The energy content (entirely mechanical, in this case) of the gas in motion is therefore equal to the energy released at t=0. This equality allows one to obtain a relation between the shock speed and the quantity  $E_0$ .

When a magnetic field is present, the situation is not quite so simple. One minor point is that, although the mechanical energy of the gas is initially negligible, the magnetic energy is not (being infinite, in fact) and must therefore be taken into account. Secondly, while the total mechanical energy of the gas in motion is still constant in time (as is also the magnetic energy), this energy can no longer be identified with the energy released at t = 0. Because of the coupling between gas and magnetic field, some fraction (not known a priori) of the energy E<sub>0</sub> appears as mechanical energy and some fraction as magnetic energy. Finally, the system is no longer isolated from external sources; it is coupled to an external circuit, which, moreover, is required to maintain a constant current. It is conceivable that such a boundary condition on the circuit implies an exchange of energy at t = 0 between external source and system. That this is in fact the case will be shown below.

As noted above, the mechanical energy and the magnetic energy are both constant between any two similarity lines. Another quantity, closely related to the latter, is also constant between any two lines of constant  $\eta$ , viz., the magnetic flux. Although the total magnetic flux between shock and axis is constant in time subsequent to the explosion, it is not, however, equal to the total magnetic flux in the same volume prior to the explosion; there has been a change in flux (per unit length),  $\Delta \bar{\tau}$ , in this volume given by

$$\Delta \theta = \int_{0}^{\mathbf{r}_{g}(\mathbf{t})} \left[ B_{0} - \frac{\mu I_{0}}{2\pi \mathbf{r}} \right] d\mathbf{r}$$

$$= 2\pi \rho_{0} c^{2\pi} \frac{\beta_{0}}{I_{0}} \int_{0}^{1} \left( \frac{\beta}{\rho^{1/2}} - \beta_{0} \right) \frac{d\rho}{(\sigma - \rho)}. \tag{30}$$

Since the flux between shock and axis is constant in time, it follows that an amount of flux,  $\Delta \bar{v}$ , is supplied (or withdrawn) at the axis at the time t=0, when shock and axis coincide. Associated with this flux is a quantity of energy (per unit length),  $\Delta E_{\rm c} = I_{\rm o} \Delta \bar{v}$ , which is supplied to (or withdrawn from) the system at t = 0 by the source maintaining the constant current  $I_{\rm o}$ . The increment in the total energy of the system thus contains a part  $\Delta E_{\rm c}$  in addition to the part  $E_{\rm c}$  released along the axis at t = 0.

The increment in the total energy of the system appears in two forms: an increment,  $\Delta E_{G}$ , in the mechanical energy, given by

$$\Delta E_{G} = 2\pi \rho_{o} c^{*2} \int_{0}^{1} \left[ \frac{P}{(\gamma - 1)} + \frac{1}{2} \sigma U^{2} \right] \frac{d\phi}{\phi(\sigma - \phi)}$$
 (31a)

and an increment,  $\Delta E_{R}$ , in the magnetic energy, given by

$$\Delta E_{\rm B} = 2\pi \rho_{\rm o} c^{*2} \int_{0}^{1} \frac{1}{2} \left[ \frac{\beta^{2}}{\phi} - \beta_{\rm o}^{2} \right] \frac{d\phi}{(\sigma - \phi)}. \tag{31b}$$

The energy balance equation for the system then becomes

$$E_{O} = \Delta E_{G} + \Delta E_{B} - \Delta E_{C}$$
 (32)

In Eq. (32), the quantity  $\Delta E_{B}$  -  $\Delta E_{C}$  represents that part of  $E_{O}$  which appears as magnetic energy.

The energy equation can be written in the form

$$E_o = 2\pi\rho_o c^{*2} \ln(\beta_o; \gamma)$$
 (33)

where  $\text{In}(\beta_0;\gamma)$  is a constant which depends on the parameter  $\beta_0$  and the specific heat ratio  $\gamma$ , and which can be evaluated only after the complete integration of the equations of motion. It is this equation which enables one to obtain the dependence of the shock speed (which is related to c) on the explosive energy  $E_0$  and the Alfvén number  $\beta_0$ .

In his treatment of the modified hydrodynamic case, Greenspan calculated  $\text{In}(\beta_0; \gamma)$  only in the limit  $\beta_0 = 0$ , where  $E_0 = \Delta E_0$ .

#### VIII. RESULTS AND CONCLUSIONS

The results of the numerical calculation of the energy parameters are shown in Figs. 5 and 6. The dependence of the quantity  $In(\beta_0;\gamma)$  on  $\beta_0$  is shown, for two different values of  $\gamma$ , in Fig. 5. In the modified hydrodynamic case,  $In(\beta_0;\gamma)$  increases monotonically from the ordinary blast wave value at  $\beta_0 = 0$  to the asymptotic value found by Greenspan at  $\beta_0 = 0$ . This implies, from Eqs. (33) and (7), that, for a given explosive energy, the shock speed decreases with increasing magnetic field. The strength of the shock, however, remains constant in this case. In the pure MHD case,  $In(\beta_0;\gamma)$  increases from the blast wave value at  $\beta_0 = 0$  to a maximum at a  $\beta_0$  of about 0.2, and then decreases to zero at  $\beta_0 = 1$ . For a given energy release in this case, then, the shock becomes weaker with increasing magnetic field, but the shock speed first decreases to a minimum value and then increases as the magnetic field is increased.

Fig. 6 shows the dependence on  $\beta_0$  of the fraction of  $E_0$  which appears as mechanical energy. In the pure MHD case, this fraction decreases monotonically from unity at  $\beta_0 = 0$  to 1/2 at  $\beta_0 = 1$ . In the weak shock limit, then, there is equipartition of the explosive energy between mechanical and magnetic energy. This is in contrast to the modified hydrodynamic case where this fraction is essentially unity, independent of  $\beta_0$ . Actually, this quantity decreases by about one half of one per cent at a value of  $\beta_0$  of about 0.5, but the decrease is too small to be shown in the figure. The explosive energy, therefore, appears almost entirely as mechanical energy in the modified hydrodynamic case.

There are some other interesting differences in energy content in the pure MFD and modified hydrodynamic cases which may be inferred from Eqs. (50)

and (31), taken together with Eqs. (24) and (29) and the discussion pertaining thereto. In the pure MHD case, where the field is everywhere compressed behind the shock, the quantities  $\Delta E_{\rm B}$  and  $\Delta E_{\rm C} = I_{\rm O}$  At are both positive. Both quantities are, in fact, positively infinite; the appearance of this divergence and its effect on the validity of the results has been discussed in the Introduction. The difference,  $\Delta E_{\rm B} - \Delta E_{\rm C}$ , is, however, finite and positive; it represents the portion of  $E_{\rm O}$  which is converted to magnetic energy at t=0. Since  $\Delta E_{\rm B} > \Delta E_{\rm C}$ , this part of  $E_{\rm O}$  appears in the compressed magnetic field between shock and axis.

In the modified hydrodynamic case, where the field is everywhere expanded behind the shock, both  $\Delta E_{\rm B}$  and  $\Delta E_{\rm c}$  are negative (although finite, in this case). The difference,  $\Delta E_{\rm B}$  -  $\Delta E_{\rm c}$ , is, however, again positive, and again represents the portion of  $E_{\rm o}$  which is converted to magnetic energy at t = 0. However, since  $\Delta E_{\rm B} < E_{\rm c}$ , this part of  $E_{\rm o}$  does not appear now in the magnetic field behind the shock but is delivered instead to the external circuit.

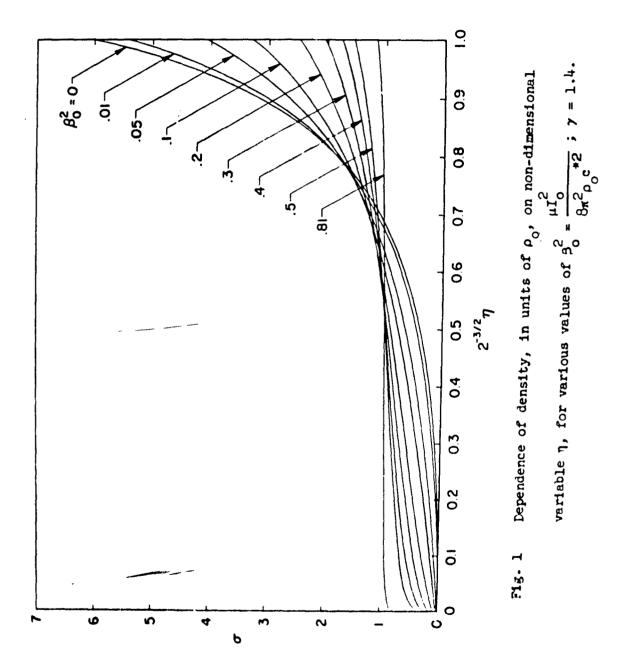
The difference just discussed implies a corresponding difference in the voltage induced in the external circuit by the gas in motion. In the pure MHD case,  $\Delta E_{\rm c}$  is positive; i.e., the external source supplies a pulse of energy at t = 0. Thus, a positive voltage pulse (i.e., in the same sense as  $I_{\rm o}$ ) should be induced in the circuit at t = 0. Subsequently, as the shock progresses outward through the gas, amb! int magnetic energy enters the region behind the shock. Since the total magnetic energy (and magnetic flux) between the shock and the axis remains constant in time, magnetic energy must leave at the axis at the same rate it is entering at the shock. Thus, the short positive voltage pulse should be followed by a long negative voltage pulse.

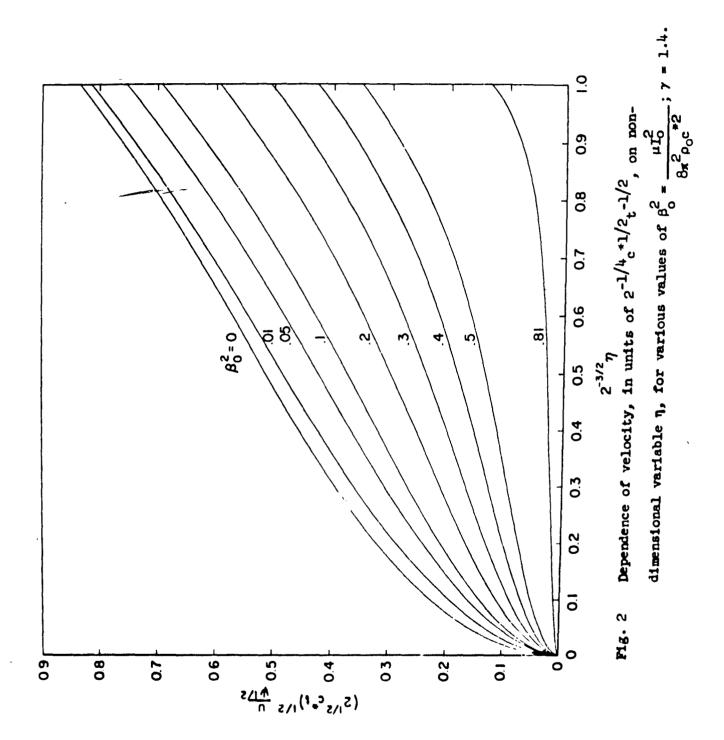
In the modified hydrodynamic case, the situation is just reversed. The quantity  $\Delta E_{\rm c}$  is now negative, which means that a pulse of energy is delivered to the circuit at t = 0. This implies an initial negative voltage pulse. As the shock progresses outwards, it "pushes out" some of the magnetic field from the gas through which it passes (the field is expanded as a result of the passage of the shock). There is thus an outflow of magnetic energy through the shock which must be balanced by an influx of energy at an equal rate at the axis. The short negative voltage pulse should therefore be followed by a long positive voltage pulse.

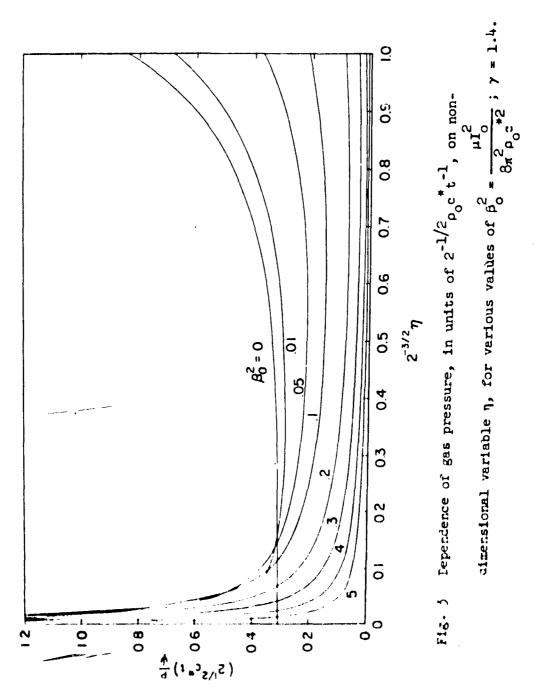
The long voltage pulses discussed above should be observable experimentally. However, whether or not the short voltage pulses would also be seen is an open question. As mentioned in the Introduction, one would expect that, in any actual experiment, where the axial conductor has a finite radius, the true flow would approach that given by the similarity solution at distances from the axis much greater than the radius of the conductor. The short voltage pulse at t = 0, however, is a property of the solution which is associated with the axis itself, and one may reasonably wonder whether this feature of the solution would be retained in an actual experiment.

Finally, the energy and flux considerations outlined above help to account, at least heuristically, for the difference in the pressure distribution at the axis in the two cases. One can think of an imaginary interface at the axis across which there must be a pressure balance if the flow is not to separate from the axis. In the pure MHD case, an infinite magnetic pressure is produced on one side of this interface by the addition of magnetic flux at t = 0; this is balanced by an infinite gas pressure

at the axis. In the modified hydrodynamic case, a "partial magnetic vacuum" is created at the axis by the removal of flux at t = 0; pressure balance in this case requires that the gas pressure be zero at the axis.







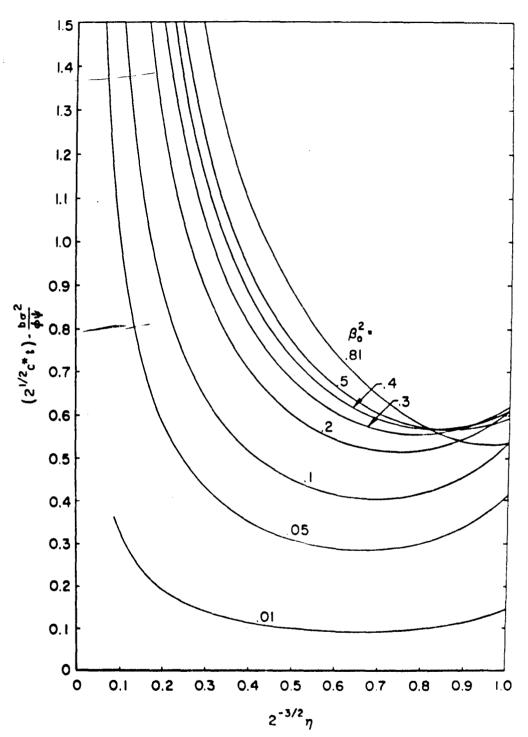


Fig. 4 Dependence of magnetic pressure, in units of  $e^{-1/2}\rho_0 e^+ t^{-1}$ , on non-dimensional variable  $\eta$ , for various values of  $\beta_0^2 = \frac{\mu \Gamma_0^2}{8\pi^2\rho_0 e^{-2}}$ ,  $\chi = 1.4$ .

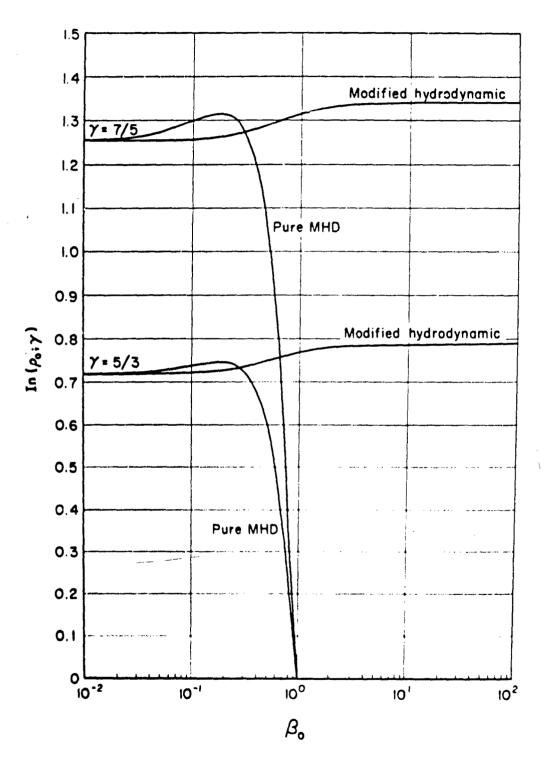
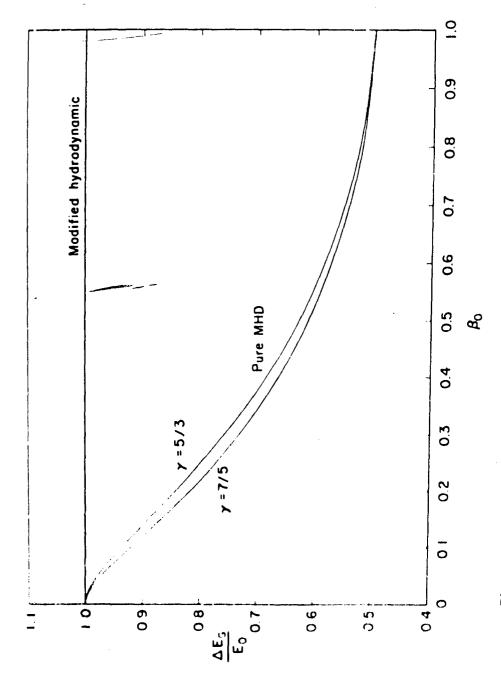


Fig. 5 Dependence of the shock speed parameter,  $In(3_0; 7)$ , on 8.



Lependence on  $\beta_0$  of the fraction of the explosive energy which appears as mechanical energy. F15. C

#### REFERENCES

- 1. Lin, S. C., "Cylindrical Shock Waves Produced by Instantaneous Energy Release," J. Appl. Phys., Vol. 25, 1954, p. 54.
- Korobeinikov, V. P., "One-dimensional Self-similar Motions of a Conducting Gas in a Magnetic Field," <u>DAN USSR</u>, Vol. 121, No. 4, 1958.
- 3. Pai, S. I., "Cylindrical Shock Waves Produced by Instantaneous Energy Release in Magneto-Gas Dynamics," Air Force Office Scientific Research, AFOSR TN 58-215, 1958.
- 4. Greenspan, H. P., "Similarity Solution for a Cylindrical Shock-Magnetic Field Interactions," Phys. Fluids, Vol. 5, 1962, p. 255.
- 5. Greifinger, C. and J. D. Cole, "On Cylindrical Magnetohydrodynamic Shock Waves," Phys. Fluids, Vol. 4, 1961, p. 527.